

**AMENDMENTS TO THE SPECIFICATION**

**IN THE SPECIFICATION:**

Please replace the paragraph bridging pages 37-38 with the following rewritten paragraph:

The conductive roller can be produced by using conventional methods. For example, the conductive elastomer composition (kneaded components) is preformed tubularly with a single-axis extruder. Then the preform is vulcanized at 160°C for 15 to 70 minutes. Thereafter a metal shaft is inserted into a hollow portion of the vulcanized tube. After the surface of the tube is polished, the tube is cut to a predetermined size to obtain a roller. An optimum vulcanizing time period should be set by using a vulcanization testing rheometer (for example, ~~Curelastmeter~~ Curelastometer). The vulcanization temperature may be set around 160°C in dependence on necessity. To suppress the stain of the photosensitive member and reduce the compression set of the conductive elastomer composition, it is preferable to set conditions of the vulcanization temperature and the vulcanization time period appropriately so that sufficient vulcanization can be accomplished. The conductive polymer composition may be vulcanized in a vulcanizing can pressurized by water vapor. It is possible to carry out a successive vulcanization method in dependence on a mixing ratio. A secondary vulcanization may be performed as

necessary. The electric resistance value of the conductive roller is favorably not less than  $10^{3.5}\Omega$  nor more than  $10^{11.0}\Omega$  and more favorably not less than  $10^{4.0}\Omega$  nor more than  $10^{9.0}\Omega$ , and most favorably not less than  $10^{4.5}\Omega$  nor more than  $10^{8.5}\Omega$ , when a voltage of 1000V is applied thereto.

On page 68 (lines 8-16), please replace the 1<sup>st</sup> full paragraph with the following rewritten paragraph:

Vulcanizing conditions are determined by a ~~Curelastmeter~~ Curelastometer or the like and adjusted appropriately to 95% torque rise time period t<sub>95</sub> minutes as a guide.

On page 82, please replace the only full paragraph (lines 2-22) with the following rewritten paragraph:

As the polymer composing the uncontinuous phase, the EO-PO-AGE copolymer was used in the examples 1 through 4 and the example 6, and the epichlorohydrin rubber was used in the example 5. The salt 1 consisting of lithium-bis (trifluoromethanesulfonyl) imide or the salt 2 consisting of lithium-tris (trifluoromethanesulfonyl) methide was distributed to the EO-PO-AGE copolymer and the epichlorohydrin rubber. The lithium-bis (trifluoromethanesulfonyl) imide and the lithium-tris (trifluoromethanesulfonyl) methide are the salt capable of dissociating into cations and anions. The low-nitrile NBR was used to form the continuous phase in the examples 1

through 6. In the examples 1 through 4, the EPDM was used to form the other uncontinuous phase (the second uncontinuous phase). Except the conductive roller of the example 2, the conductive rollers of the other examples was formed as rollers having a layer made of cellular material. The salt 2 had an electric conductivity of 3.6 mS/cm, when the electric conductivity was measured at a concentration of a salt of 0.1 mol/liter at 25°C in a mixed solvent of propylene carbonate (PC) and dimethyl carbonate (DME) (mixing ratio between PC and DME is 1:2 in volume fraction).

On page 94, please replace the last full paragraph (lines 16-23) with the following rewritten paragraph:

Regarding the conductive belt of each of the examples 12 through 17 and the comparison examples 11 through 16, a cut piece of the obtained conductive belt, a laser beam printer DocuPrint 180 manufactured by Fuji Xerox Co., Ltd., and a photosensitive member set on a cartridge (commodity code: CT350035) of the printer were used to evaluate the degree of stain of the photosensitive member. The conductive belts with pressed against the photosensitive member were stored at 45°C and a relative humidity of 80%.

On page 108, please replace the 2<sup>nd</sup> full paragraph (lines 8-23) with the following rewritten paragraph:

The volume resistivity ~~value~~ of each conductive belt was measured at a constant temperature of 23°C and a constant relative humidity of 55% in the same state as the state in which the volume specific resistance is measured. A constant voltage of 1000V was applied successively for five hours to a point inside the conductive belt having a thickness of 0.25mm by using the ultra-high resistance meter R-8240A manufactured by Advantest Corporation. The volume resistivity  $\rho_v$  (t=0 hour) of the belt immediately after a constant voltage of 1000V is applied to the belt is measured. The volume resistivity  $\rho_v$  (t=five hours) after the voltage is applied to the belt for five hours successively is also measured. By using the obtained values, the rise amount of the volume resistivity during successive energization was computed in accordance with the following equation:

$$\Delta \log_{10} \rho_v (t=5-0 \text{ hour}) (\Omega \cdot \text{cm}) = \log_{10} \rho_v (t=\text{five hours}) - \log_{10} \rho_v (t=0 \text{ hour}).$$

Tables 5 through 7 show the results.

On page 109, please replace the 1<sup>st</sup> full paragraph (lines 10-17) with the following rewritten paragraph:

As shown in Table- 5, the belt of each of the examples 12 and 13 had excellent electric characteristic and did not have the problem of migration stain to the photosensitive member because the salt capable of dissociating into cations and anions was distributed to the first uncontinuous phase. Especially, each belt

had a low degree of dependence of its electric resistance on environment and a small value in the rise of the electric resistance during energization.

Please replace the paragraph bridging pages 110-111 with the following rewritten paragraph:

The example 16 was similar to the example 12 in its specification except that as the salt capable of dissociating into cations and anions, instead of the salt 1 used in the example 12, the salt 5 was used in the example 16. Though the cation of the salt 5 is heavier than that of the salt 1. ~~The~~, the belt of the example 16 had a sufficient electric conduction similarly to the example 14. Then the belt of the example 16 had a small value in the rise of its volume resistivity during successive energization. Further the volume specific resistance of the belt of the example 16 had a low degree of dependence on environment.

Please replace the paragraph bridging pages 118-119 with the following rewritten paragraph:

50 wt% of melamine cyanurate (MC640 produced by Nissan ~~chemical Industries, Ltd~~ Chemical Industries, Ltd.) was dry-blended with a polyester thermoplastic elastomer ("Pelprene P90BD" produced by ToyoBo Co., ~~ltd~~ Ltd.: polyester polyether type (glass transition temperature  $T_g$ :  $-56^{\circ}\text{C}$ )). The mixture was supplied to the hopper,

namely, the biaxial extruder to knead it at 210°C. Thereby a flame-retardant master batch was obtained. The temperature of the resin measured at this time was 230°C.

Please replace the paragraph bridging pages 119-120 with the following rewritten paragraph:

The material for the belt was supplied to the hopper(51) of the extrusion unit of the belt-manufacturing apparatus shown in Fig. 10. The extrusion unit was operated to fuse the material. The fused material was extruded vertically downward from the annular die having a temperature of 235°C. The annular die has an inner diameter of 185mm and a gap of 0.5mm. The fused material was fed along the inside sizing unit having an outer diameter of 170mm to cool it at 80°C. As a result, the material was ~~turned~~ formed into a tube by cooling. Then the material was drawn vertically downward at a take-off speed of 1m/minute. Then the material was cut by the automatic cutting unit. As a result, the material had a width of 40mm. In this manner, the flame-retardant seamless belt is successively obtained. The belt had an inner diameter of 169.5mm, a thickness of 250 $\mu$ m, and a width of 400mm.